

Optics of Anisotropic Media

Introduction

Aim of this course

- Introduction to physical principles of polarization optics,
- Electromagnetic waves in different media,
- Application of polarization of light in physics, optoelectronics and photonics,
 - Especially in electrooptic and magneto optic systems and optical fibers, liquid crystal cells,

Agenda

1. Maxwell equations for electromagnetic waves in different media,
2. Mathematical description of state of polarization:
 - a. Trigonometric method,
 - b. Jones vectors,
 - c. Coherence matrix for quasi-monochromatic electromagnetic wave,
 - d. Stokes vector,
 - e. Poincare sphere,
3. Electromagnetic wave in anisotropic media,
4. Anisotropic media:
 - a. Types of anisotropic media,
 - b. Piezo-optic and elasto-optic phenomena,
 - c. Electro-optic and magneto-optic effects,
5. Transformation of state of polarization:
 - a. Jones matrix, Mueller matrix,
 - b. Determination of SOP changes using Poincare sphere,
6. Application of anisotropic media in technics,
 - a. Methods of SOP generation and measurement,
 - b. Polariscopy
 - c. Compensators,
 - d. Conoscopy,
 - e. Lyott filters,

Recommended literature:

1. Florian Ratajczyk, **Optyka ośrodków anizotropowych** , PWN
(lub **Dwójłomność i polaryzacja optyczna**, OFPWr)
2. D. Goldstein, **Polarized Light**, M. Dekker, New York, 2003
3. E. Collet, **Polarization light in fiber optics**, PolaWave Group, Lincroft 2003
4. C. Brosseau, **Fundamentals of Polarized Light**, Wiley & Sons, New York ,1998
5. M.Born, E.Wolf, **Principles in Optics**, Cambridge University Press, Cambridge, 1999
6. D. J. Griffiths, **Podstawy elektrodynamiki**, PWN

Lecture 1

Mathematical basics

$$\vec{E} = [E_x, E_y, E_z]$$

$$\text{Operator } \vec{\nabla} = \vec{i} \frac{\partial}{\partial x} + \vec{j} \frac{\partial}{\partial y} + \vec{k} \frac{\partial}{\partial z}$$

$$\text{grad } \varphi = \vec{\nabla} \cdot \varphi = \vec{i} \frac{\partial \varphi}{\partial x} + \vec{j} \frac{\partial \varphi}{\partial y} + \vec{k} \frac{\partial \varphi}{\partial z}$$

Divergence of vector -> a quantity of a vector field's source at each point,

$$\text{div } \vec{E} = \vec{\nabla} \cdot \vec{E} = \frac{\partial E_x}{\partial x} + \frac{\partial E_y}{\partial y} + \frac{\partial E_z}{\partial z}$$

Curl -> infinitesimal rotation of 3-dimensional vector field

$$\text{rot } \vec{E} = \vec{\nabla} \times \vec{E} = \begin{vmatrix} \vec{i} & \vec{j} & \vec{k} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ E_x & E_y & E_z \end{vmatrix}$$

Laplace operator $\Delta = \frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2} + \frac{\partial^2}{\partial z^2}$

$$\vec{\nabla} \times (\vec{\nabla} \times \vec{E}) = \vec{\nabla} \vec{\nabla} \vec{E} - \nabla^2 \vec{E} = \vec{\nabla} \vec{\nabla} \vec{E} - \Delta \vec{E}$$

Divergence theorem (Gauss – Ostogradsky theorem)

$$\int_V (\nabla \cdot \vec{v}) d\tau = \oint_S \vec{v} \cdot d\vec{a}$$

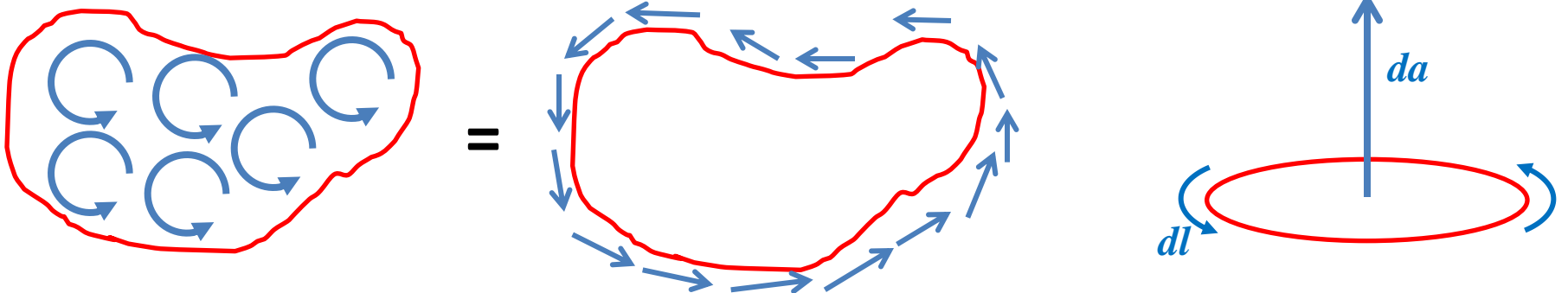
Interpretation: The outward flux of a vector field through a closed surface is equal to the volume integral of the divergence over the region inside the surface.

Moreover, *sum of all sources minus the sum of all sinks gives the net flow out of a region.*

Kelvin-Stokes theorem (curl theorem)

$$\int_S (\vec{\nabla} \times \vec{v}) \cdot d\vec{a} = \oint_P \vec{v} \cdot d\vec{l}$$

Interpretation: The integral of the curl of the vector field over some surface is equal to the line integral of the vector field around the boundary of the surface.



Maxwell's equations for isotropic media

Maxwell's equations

$$\text{rot}\vec{H} - \dot{D} = \sigma\vec{E}$$

$$\text{rot}\vec{E} + \dot{B} = 0$$

$$\text{div}\vec{D} = \rho$$

$$\text{div}\vec{B} = 0$$

Material equations

$$\vec{D} = \varepsilon\varepsilon_0\vec{E}$$

$$\vec{B} = \mu\mu_0\vec{H}$$

\vec{E} Intensity of electric field[V/m]

\vec{D} Electric displacement field vector[C/m²]

\vec{H} Intensity of magnetic field [A/m]

\vec{B} Magnetic field vector [Tesla]

ρ Density of free charge


σ conductivity

Isotropic media

$$\vec{D} = \varepsilon_0 \varepsilon \vec{E}$$

$$\varepsilon = n^2$$

tensor


$$\bar{\varepsilon} = \begin{pmatrix} n^2 & 0 & 0 \\ 0 & n^2 & 0 \\ 0 & 0 & n^2 \end{pmatrix} = \begin{pmatrix} \varepsilon & 0 & 0 \\ 0 & \varepsilon & 0 \\ 0 & 0 & \varepsilon \end{pmatrix}$$

Linearly birefringent media

$$\vec{D} = \varepsilon_0 \varepsilon \vec{E}$$

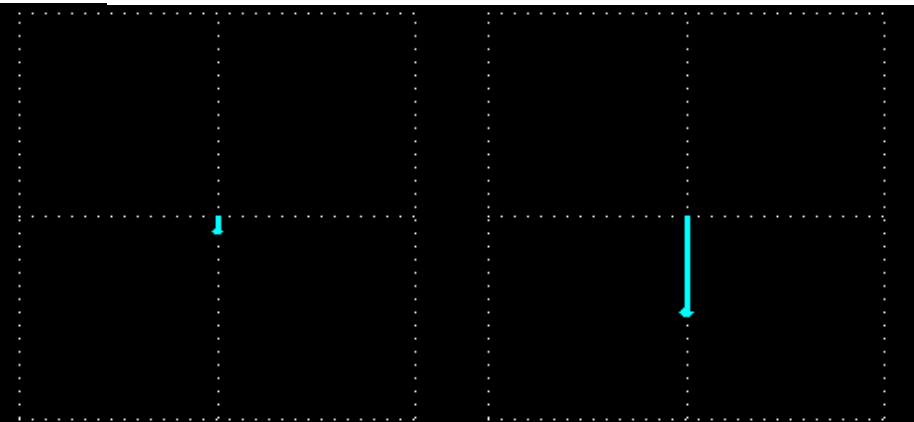
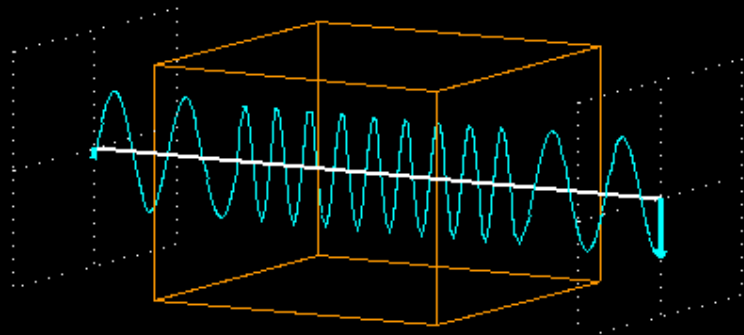
$$\varepsilon = \begin{pmatrix} n_x^2 & 0 & 0 \\ 0 & n_y^2 & 0 \\ 0 & 0 & n_z^2 \end{pmatrix} = \begin{pmatrix} \varepsilon_x & 0 & 0 \\ 0 & \varepsilon_y & 0 \\ 0 & 0 & \varepsilon_z \end{pmatrix}$$

Elliptically birefringent media

Isotropic medium

In

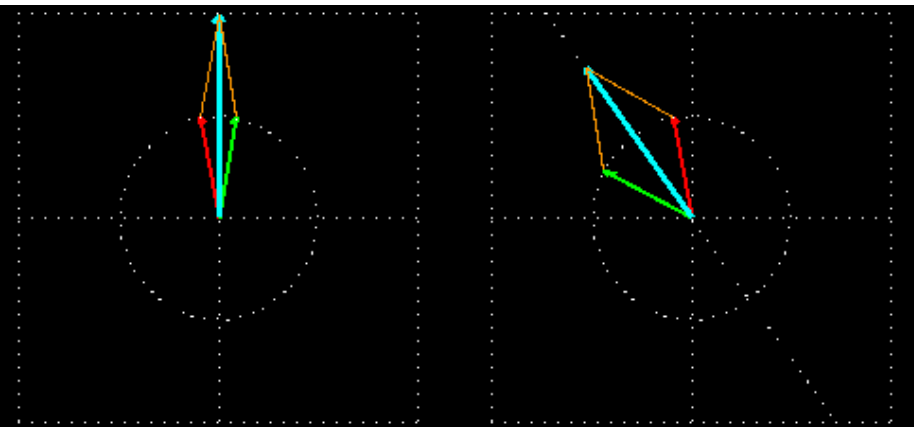
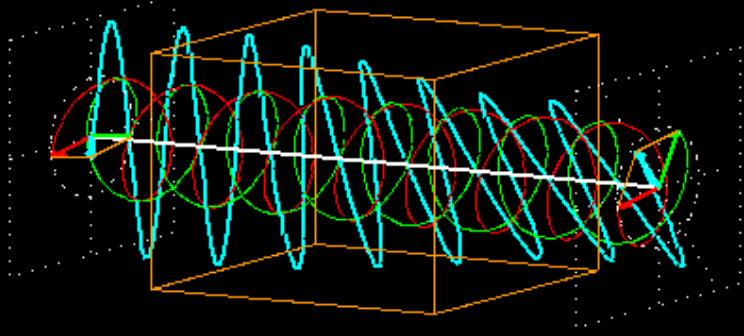
Out



Elliptically birerfingent medium

In

Out



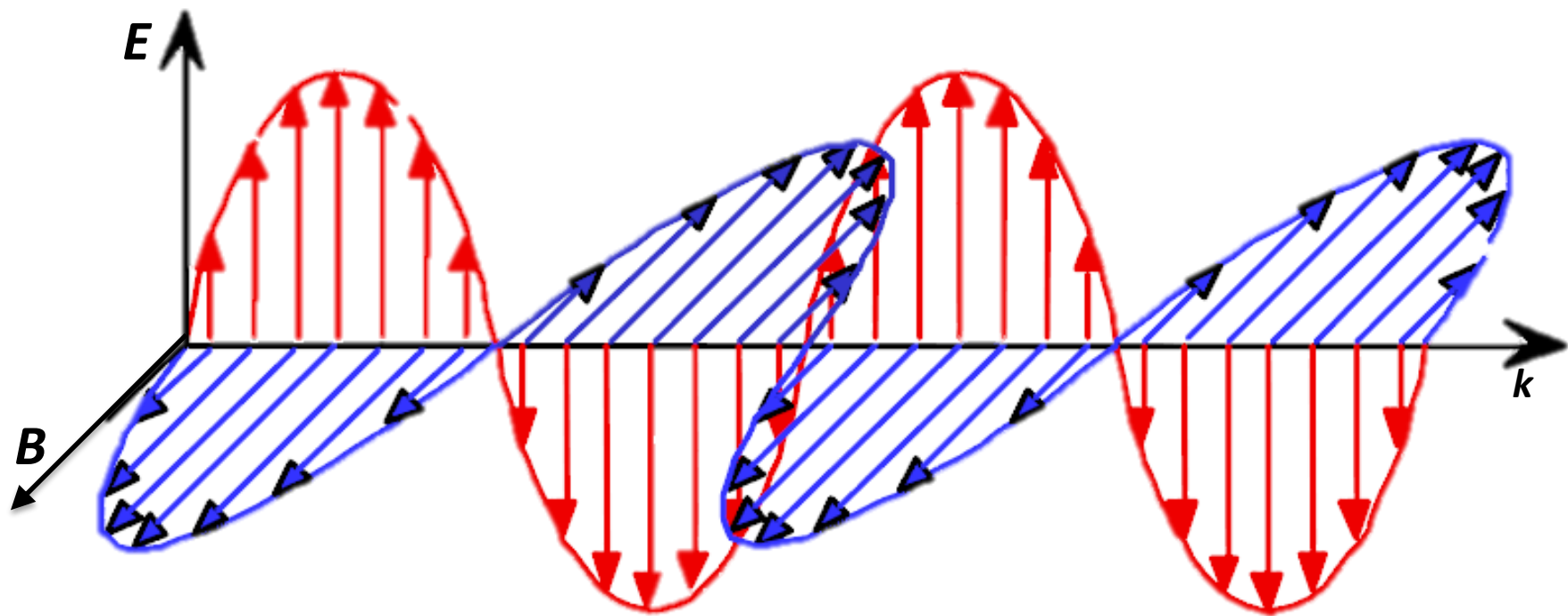
$$E_x = E_{0x} \exp \left[i\omega \left(t - \frac{z}{c_n} \right) \right]$$
$$E_y = E_{0y} \exp \left[i\omega \left(t - \frac{z}{c_n} \right) \right]$$

1. Electromagnetic wave is a transverse wave,
2. Is a plane wave (amplitude m is independent on z coordinate)
3. Vectors E i H are orthogonal to each other,
4. ... and oscillates at the same phase,

6. The energy is transported perpendicularly to the wavefront
(but only in anisotropic medium!)

$$\vec{S} = \vec{E} \times \vec{H}$$

7. Refractive index is a dispersive quantity,



Methods of describing state of polarization for light

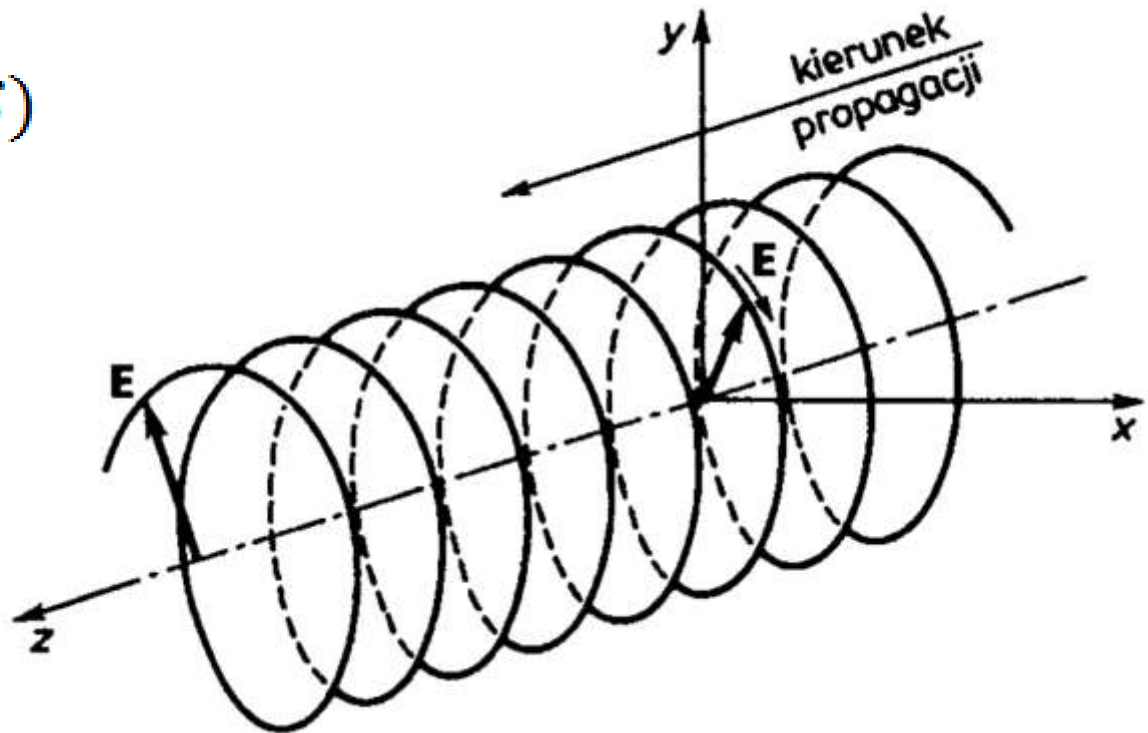
Trigonometric method

$$E_x = m_x \exp \left(i \left[\omega t - \left(\frac{\omega Z}{c_n} + \delta_{0x} \right) \right] \right) = m_x \exp(\omega t - \delta_x)$$

$$E_y = m_y \exp \left(i \left[\omega t - \left(\frac{\omega Z}{c_n} + \delta_{0y} \right) \right] \right) = m_y \exp(\omega t - \delta_y)$$

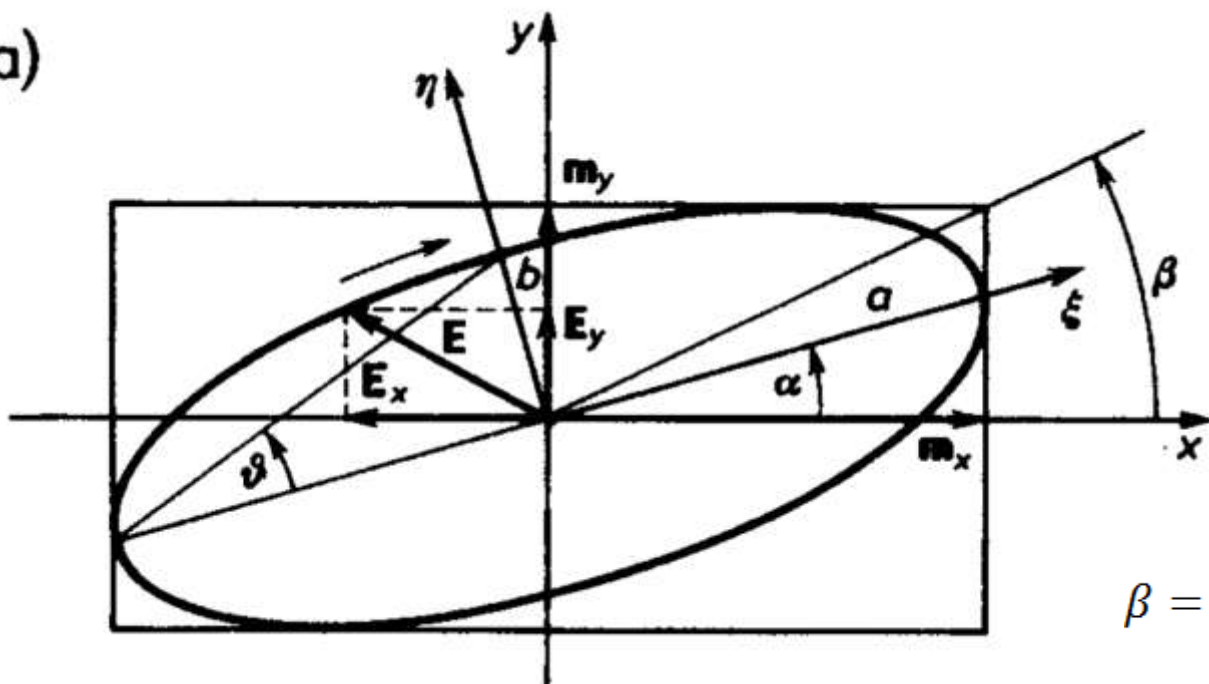
$$E_x = m_x \cos(\omega t)$$

$$E_y = m_y \cos(\omega t + \delta)$$



$$\left(\frac{E_x}{m_x}\right)^2 - \frac{2E_x E_y}{m_x m_y} \cos(\delta) + \left(\frac{E_y}{m_y}\right)^2 = \sin^2(\delta)$$

a)



$$\beta = \arctg\left(\frac{m_y}{m_x}\right)$$

Kąt przekątnej

α

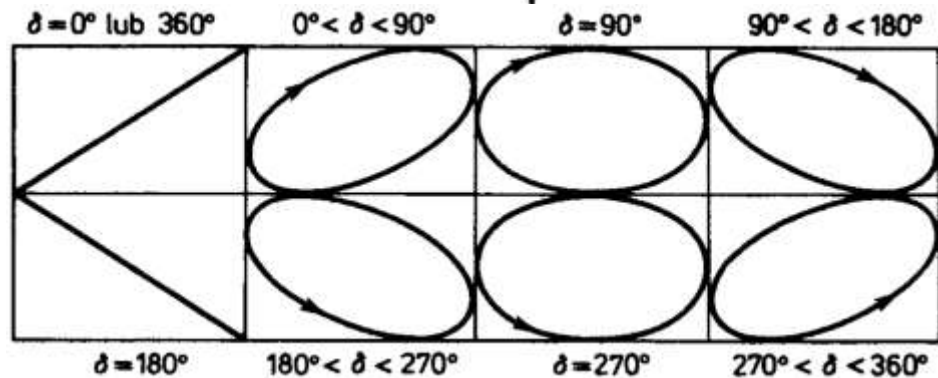
azymut

$\frac{b}{a}$

Eliptyczność

$$\vartheta = \arctg\left(\frac{b}{a}\right)$$

Kąt eliptyczności



Jones's vector

$$[E] = \begin{bmatrix} E_x \\ E_y \end{bmatrix} = e^{i\omega t} \begin{bmatrix} m_x \\ m_y e^{i\delta} \end{bmatrix}$$




Or in simplified form

$$[E] = \begin{bmatrix} E_x \\ E_y \end{bmatrix} = \begin{bmatrix} m_x \\ m_y e^{i\delta} \end{bmatrix}$$

Jones's vector estimation

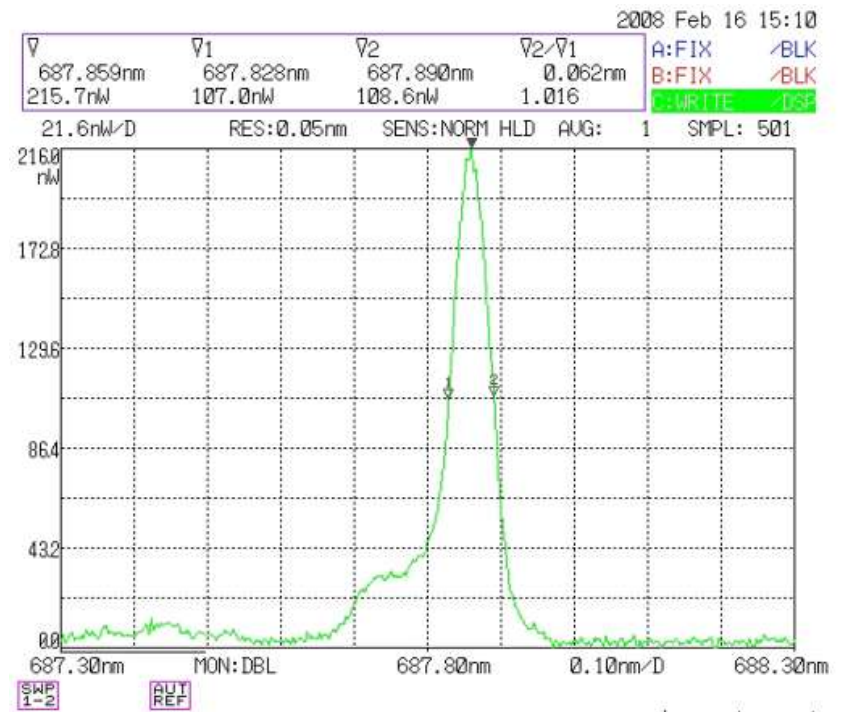
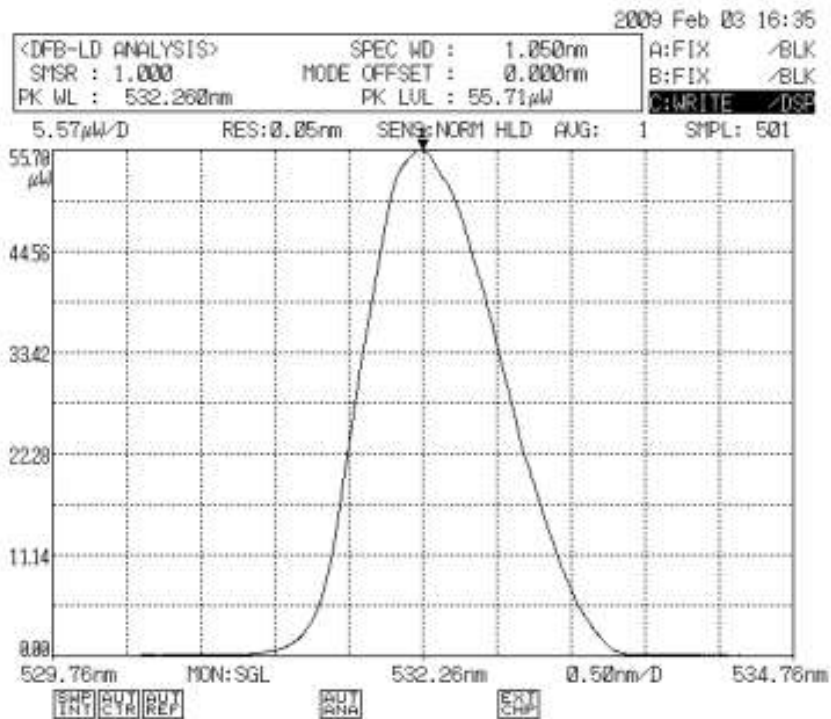
$$[E] = \begin{bmatrix} E_x \\ E_y \end{bmatrix} = \begin{bmatrix} m_x \\ m_y e^{i\delta} \end{bmatrix}$$

- Light intensity for X and Y axis through polarizer,
- Phase angle δ through compensator,

Symbol	Azymut	Kąt eliptyczności	Standardowy wektor Jonesa	Pełny wektor Jonesa
—	0°	0°	$\begin{bmatrix} 1 \\ 0 \end{bmatrix}$	$\begin{bmatrix} m_x \\ 0 \end{bmatrix}$
	90°	0°	$\begin{bmatrix} 0 \\ 1 \end{bmatrix}$	$\begin{bmatrix} 0 \\ m_y \end{bmatrix}$
/	45°	0°	$\frac{\sqrt{2}}{2} \begin{bmatrix} 1 \\ 1 \end{bmatrix}$	$\begin{bmatrix} m_x \\ m_x \end{bmatrix}$
\	-45°	0°	$\frac{\sqrt{2}}{2} \begin{bmatrix} 1 \\ -1 \end{bmatrix}$	$\begin{bmatrix} m_x \\ -m_x \end{bmatrix}$
polaryzacja liniowa ogólnie		0°	$\begin{bmatrix} \cos\beta \\ \pm \sin\beta \end{bmatrix}$	$\begin{bmatrix} m_x \\ \pm m_y \end{bmatrix}$
	-	-45°	$\frac{\sqrt{2}}{2} \begin{bmatrix} 1 \\ -i \end{bmatrix}$	$\begin{bmatrix} m_x \\ m_x e^{-i\pi/2} \end{bmatrix}$
	-	45°	$\frac{\sqrt{2}}{2} \begin{bmatrix} 1 \\ i \end{bmatrix}$	$\begin{bmatrix} m_x \\ m_x e^{i\pi/2} \end{bmatrix}$
	0°	26,57°	0,89 $\begin{bmatrix} 0,5 \\ i \end{bmatrix}$	$\begin{bmatrix} m_x \\ 2m_x e^{i\pi/2} \end{bmatrix}$
polaryzacja eliptyczna ogólnie	α	β	$\begin{bmatrix} \cos\beta \\ \sin\beta e^{i\delta} \end{bmatrix}$	$\begin{bmatrix} m_x \\ m_y e^{i\delta} \end{bmatrix}$

Coherence matrix

For quasi-monochromatic wave



Coherence matrix

$$[K] = \begin{bmatrix} \mathbf{I}_{xx} & \mathbf{I}_{xy} \\ \mathbf{I}_{yx} & \mathbf{I}_{yy} \end{bmatrix} = \begin{bmatrix} \langle E_x E_x^* \rangle & \langle E_x E_y^* \rangle \\ \langle E_y E_x^* \rangle & \langle E_y E_y^* \rangle \end{bmatrix}$$

Light intensity:

$$I = \text{Tr}[K]$$

Polaryzacja eliptyczna

$$\det [K] = 0; \mu_{xy} = e^{i\sigma}$$

$$[K] = \begin{bmatrix} m_x^2 & m_x m_y e^{i\delta} \\ m_x m_y e^{-i\delta} & m_y^2 \end{bmatrix}$$

Polaryzacja kołowa prawoskrętna

$$[K] = \frac{I}{2} \begin{bmatrix} 1 & i \\ -i & 1 \end{bmatrix}$$

Polaryzacja kołowa lewoskrętna

$$[K] = \frac{I}{2} \begin{bmatrix} 1 & -i \\ i & 1 \end{bmatrix}$$

Polaryzacja liniowa $z = 0, 1, 2, \dots$

$$[K] = \begin{bmatrix} m_x^2 & m_x m_y (-1)^z \\ m_x m_y (-1)^z & m_y^2 \end{bmatrix}$$

- Estimation of coherence matrix elements

$$I(\theta, \delta)$$

$$I(0^\circ, 0^\circ) = I_{xx},$$

$$I(90^\circ, 0^\circ) = I_{yy},$$

$$I(45^\circ, 0^\circ) = 0,5 (I_{xx} + I_{yy} + I_{xy} + I_{yx}),$$

$$I(135^\circ, 0^\circ) = 0,5 (I_{xx} + I_{yy} - I_{xy} - I_{yx}),$$

$$I(45^\circ, 90^\circ) = 0,5 (I_{xx} + I_{yy} - iI_{xy} + iI_{yx}),$$

$$I(135^\circ, 90^\circ) = 0,5 (I_{xx} + I_{yy} + iI_{xy} - iI_{yx}).$$

$$\operatorname{Re} I_{xy} = \operatorname{Re} I_{yx} = 0,5 [I(45^\circ, 0^\circ) - I(135^\circ, 0^\circ)],$$

$$\operatorname{Im} I_{xy} = \operatorname{Im} I_{yx} = 0,5 [I(135^\circ, 90^\circ) - I(45^\circ, 90^\circ)].$$

Stokes vector

$$\mathbf{S} = \begin{bmatrix} S_0 \\ S_1 \\ S_2 \\ S_3 \end{bmatrix} = \begin{bmatrix} I_{xx} + I_{yy} \\ I_{xx} - I_{yy} \\ I_{xy} + I_{yx} \\ i(I_{yx} - I_{xy}) \end{bmatrix} = \sqrt{\frac{\epsilon_0}{\mu_0}} \begin{bmatrix} \langle E_x E_x^* \rangle + \langle E_y E_y^* \rangle \\ \langle E_x E_x^* \rangle - \langle E_y E_y^* \rangle \\ \langle E_x E_y^* \rangle + \langle E_y E_x^* \rangle \\ i(\langle E_y E_x^* \rangle - \langle E_x E_y^* \rangle) \end{bmatrix}$$

- can be applied to characterize quasi-monochromatic and partially polarized light
- Jones vector cannot be applied here,

Stokes vector

- For monochromatic wave

$$S = \begin{bmatrix} S_0 \\ S_1 \\ S_2 \\ S_3 \end{bmatrix} = \begin{bmatrix} m_x^2 + m_y^2 \\ m_x^2 - m_y^2 \\ 2m_x m_y \cos \delta \\ 2m_x m_y \sin \delta \end{bmatrix} = I_s \begin{bmatrix} 1 \\ \cos 2\beta \\ \sin 2\beta \cos \delta \\ \sin 2\beta \sin \delta \end{bmatrix} = I_s \begin{bmatrix} 1 \\ \cos 2\vartheta \cos 2\alpha \\ \cos 2\vartheta \sin 2\alpha \\ \sin 2\vartheta \end{bmatrix}$$

Stokes vector

DOP

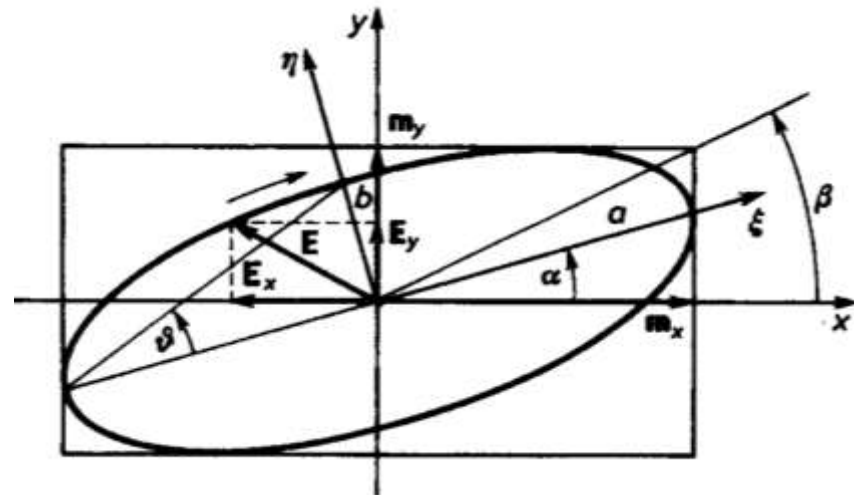
$$P = \frac{\sqrt{S_1^2 + S_2^2 + S_3^2}}{S_0} \leq 1$$










Ellipticity

$$\frac{b}{a} = \pm \tan^{-1} \left[\frac{1}{2} \sin^{-1} \left(\frac{S_3}{\sqrt{S_1^2 + S_2^2 + S_3^2}} \right) \right]$$

Azimuth

$$\alpha = \frac{1}{2} \tan^{-1} \left(\frac{S_2}{S_1} \right)$$



Symbol	Azymut	b/a	Wektor Stokesa	
*	—	—	$I\{1, 0, 0, 0\}$	światło naturalne
	0°	0	$I\{1, 1, 0, 0\}$	polaryzacja liniowa
	90°	0	$I\{1, -1, 0, 0\}$	
	45°	0	$I\{1, 0, 1, 0\}$	
	-45°	0	$I\{1, 0, -1, 0\}$	
ogólnie	α	ϑ	$I\{1, \cos 2\alpha, \sin 2\alpha, 0\}$	
	—	-1	$I\{1, 0, 0, -1\}$	polaryzacja kołowa
	—	1	$I\{1, 0, 0, 1\}$	
	0°	0,5	$I\{1, 0,6, 0, 0,8\}$	polaryzacja eliptyczna
	90°	0,5	$I\{1, -0,6, 0, 0,8\}$	
	$22,5^\circ$	0,318	$I\{1, \sqrt{1/3}, \sqrt{1/3}, \sqrt{1/3}\}$	
ogólnie	α	$\text{tg}\vartheta$	$I\{1, \cos 2\vartheta \cos 2\alpha, \cos 2\vartheta \sin 2\alpha, \sin 2\vartheta\}$	polaryzacja częściowa
ogólnie	α	$\text{tg}\vartheta$	$\{I, pI \cos 2\vartheta \cos 2\alpha, pI \cos 2\vartheta \sin 2\alpha, pI \sin 2\alpha\}$	

Poincare sphere

Graphical representation of Stokes vector

$$S_1 = I \cos 2\vartheta \cos 2\alpha,$$

$$S_2 = I \cos 2\vartheta \sin 2\alpha,$$

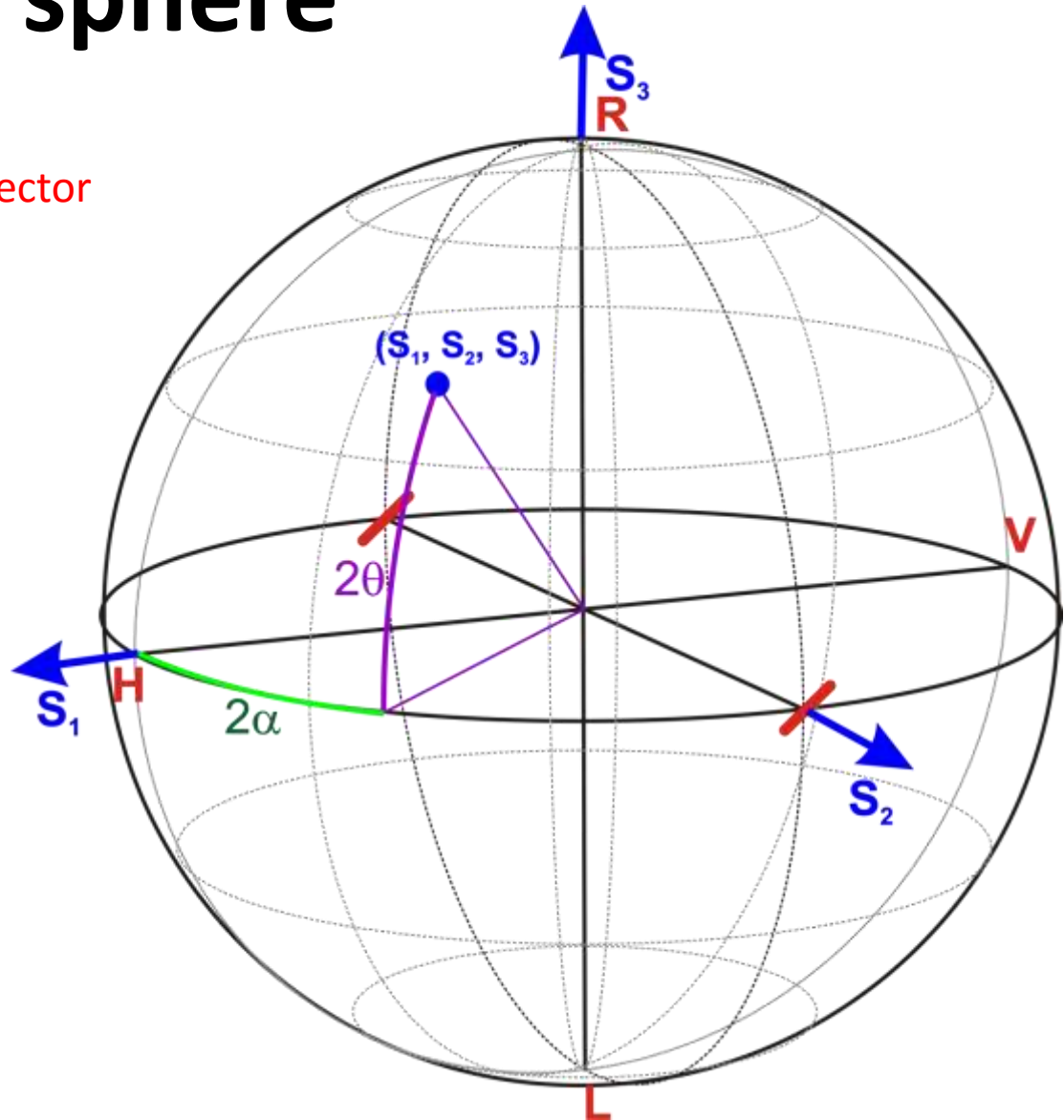
$$S_3 = I \sin 2\vartheta$$

Equator – linear states,

Meridians – states with the same azimuths,

Parallels – states with the same ellipticity,

Poles – circular polarization



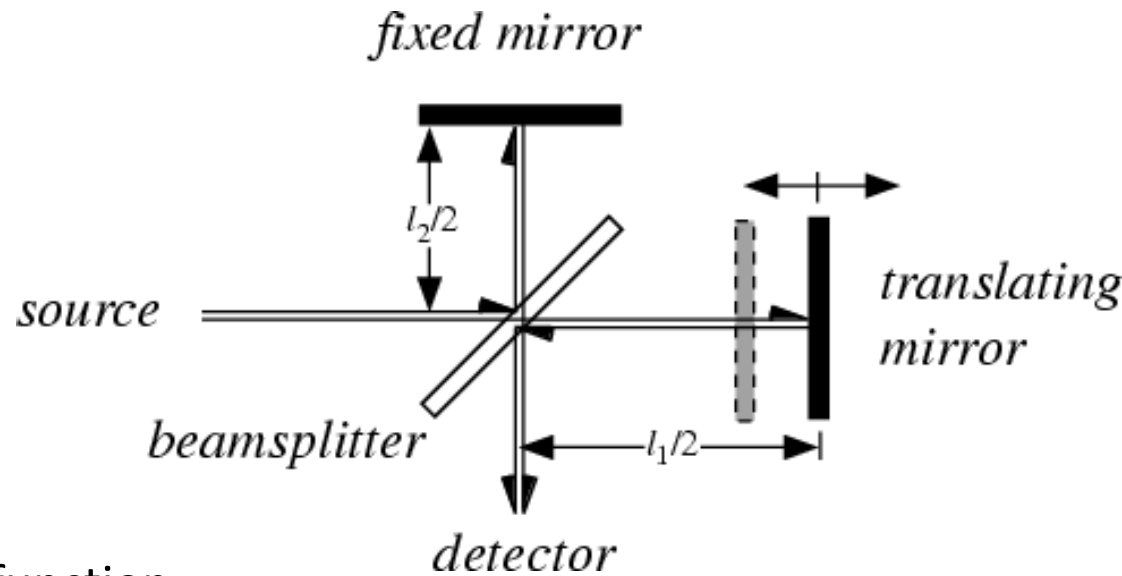
Polarization and interference

Temporar coherence

$$\Delta L = 2(l_2 - l_1) = c\tau_c$$

$$\Delta L = c\Delta t = \frac{c}{\Delta\nu} \approx \frac{\lambda^2}{\Delta\lambda}$$

Michelson's interferometer



γ_{12} - Temporar coherence function

$|\gamma_{12}|$ - Module of temporar coherence function

$$I_d = \left| \left\langle \vec{E}_1 + \vec{E}_2 \right\rangle \right|^2 = \bar{I}_1 + \bar{I}_2 + 2\sqrt{I_1 I_2} \gamma_{12}(\tau)$$

$$I = \sqrt{\frac{\epsilon_0}{\mu_0}} \langle \mathbf{E} \mathbf{E}^* \rangle = \sqrt{\frac{\epsilon_0}{\mu_0}} \langle (\mathbf{E}_1 + \mathbf{E}_2)(\mathbf{E}_1 + \mathbf{E}_2)^* \rangle = I_1 + I_2 + 2 \sqrt{\frac{\epsilon_0}{\mu_0}} \operatorname{Re} \left\{ \langle \mathbf{E}_1^* \mathbf{E}_2 \rangle \right\}$$

$$\Gamma(\tau) = \langle E_1^*(t) E_1(t + \tau) \rangle = \lim_{T_m \rightarrow \infty} \frac{1}{T_m} \int_{-T_m/2}^{T_m/2} E_1^*(t) E_1(t + \tau) dt$$

$$\gamma(\tau) = |\gamma(\tau)| \exp(i\beta_{12}) = \frac{\Gamma(\tau)}{\Gamma(0)}$$

$$I = I_1 + I_2 + 2\sqrt{I_1 I_2} |\gamma(\tau)| \cos(\beta_{12} - \Delta\delta),$$

$$\Gamma(\tau) = \int_0^{\infty} 4G(\nu) \exp(-i2\pi\nu\tau) d\nu$$

$$\gamma(\tau) = \int_0^{\infty} \hat{G}(\nu) \exp(-i2\pi\nu\tau) d\nu$$

$$\hat{G}_G(\nu) = \frac{2\sqrt{\ln 2}}{\sqrt{\pi\Delta\nu}} \exp\left[-\left(2\sqrt{\ln 2} \frac{\nu - \bar{\nu}}{\Delta\nu}\right)^2\right]$$

$$\hat{G}_L(\nu) = \frac{2(\pi\Delta\nu)^{-1}}{1 + 2\left(\frac{\nu - \bar{\nu}}{\Delta\nu}\right)^2}$$

$$\gamma_G(\tau) = \exp\left[-\left(\frac{\pi\Delta\nu\tau}{2\sqrt{\ln 2}}\right)^2\right] \exp(-i2\pi\bar{\nu}\tau)$$

$$\gamma_L(\tau) = \exp(-\pi\Delta\nu\tau) \exp(-i2\pi\bar{\nu}\tau)$$

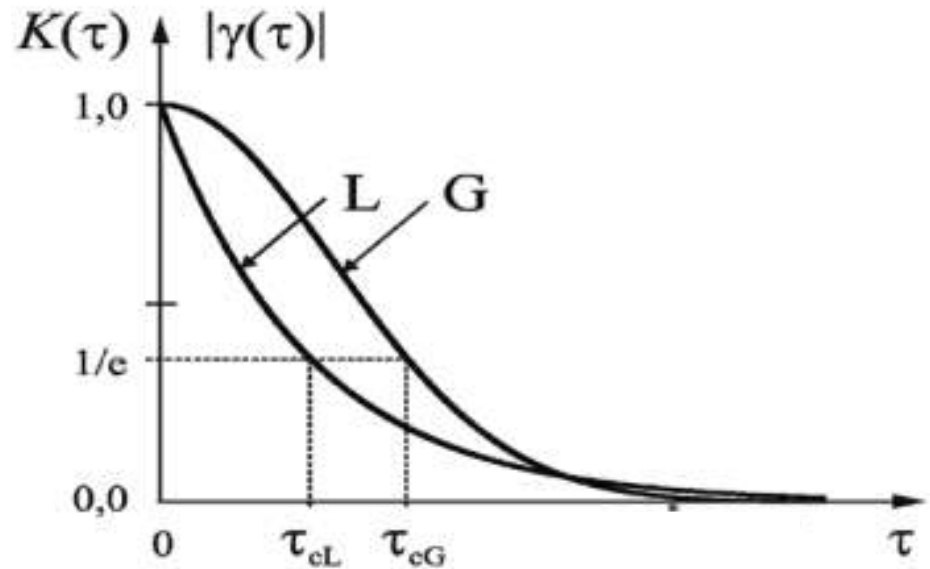
Temporal coherence of light

$$\Delta L = 2(l_2 - l_1) = c \tau_c$$

$$\Delta L = c \Delta t = \frac{c}{\Delta f} = \frac{\lambda^2}{\Delta \lambda}$$

$$K(\tau) = \frac{I_{max}(\tau_1) - I_{min}(\tau_2)}{I_{max}(\tau_1) + I_{min}(\tau_2)}$$

$$K(\tau) = |\gamma(\tau)|$$

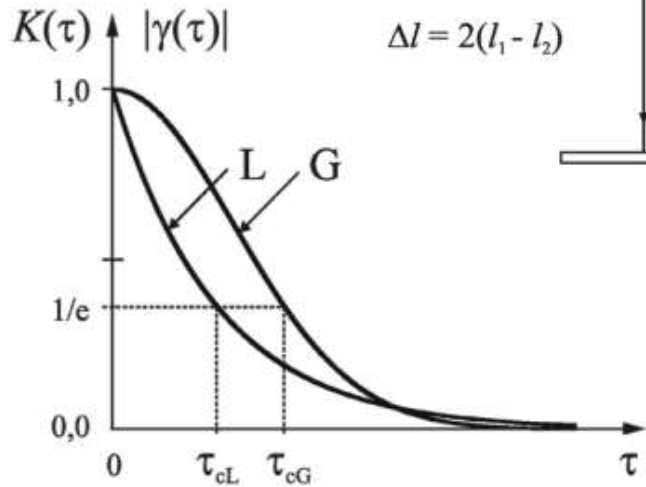
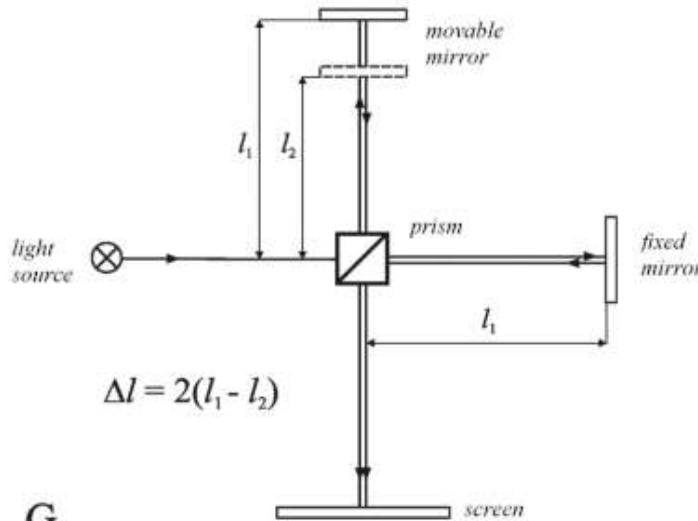


$$I_{min}(\tau_2) = 2I_1 + 2\text{Re}\{\Gamma(\tau_2)\} = 2I_1 - 2|\Gamma(\tau)|$$

$$I_{max}(\tau_1) = 2I_1 + 2\text{Re}\{\Gamma(\tau_1)\} = 2I_1 + 2|\Gamma(\tau)|$$

Koherencja czasowa

Opisuje zdolność do interferencji dwóch wiązek świetlnych z tego samego źródła, ale propagujących się w różnych kierunkach (interferometr)



τ_c - Czasowe opóźnienie kiedy kontrast spada do $\frac{1}{e}$ wartości maksymalnej

Rozkład natężenia światła można wyrazić zespolonym stopniem koherencji

$$\gamma(\tau) = |\gamma(\tau)| \exp(i\beta_{12}) = \frac{\Gamma(\tau)}{\Gamma(0)}$$

$$\tau = \frac{\Delta l}{c}$$

$$\gamma_G(\tau) = \exp\left[-\left(\frac{\pi\Delta\nu\tau}{2\sqrt{\ln 2}}\right)^2\right] \exp(-i2\pi\nu\tau)$$

$$\gamma_L(\tau) = \exp(-\pi\Delta\nu\tau) \exp(-i2\pi\nu\tau)$$

Kontrast równy jest stopniowi koherencji

$$K(\tau) = |\gamma(\tau)|$$

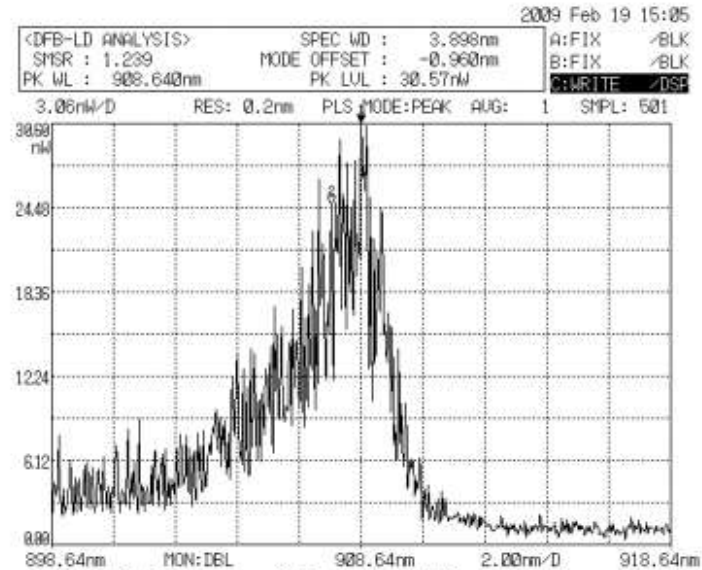
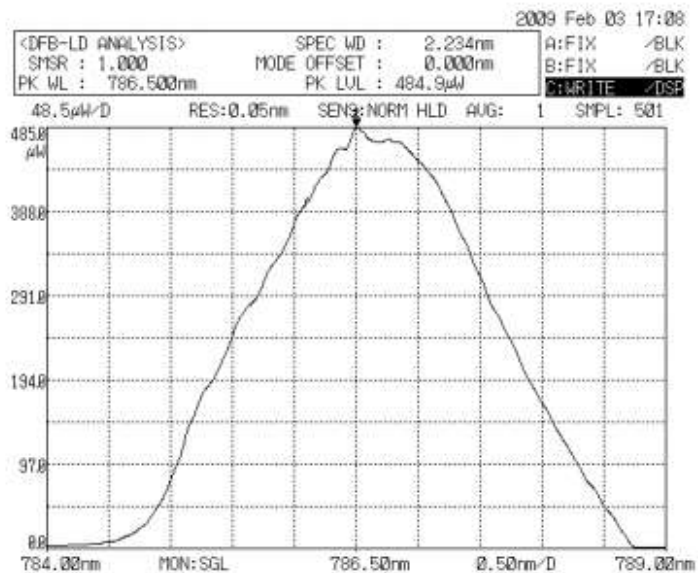
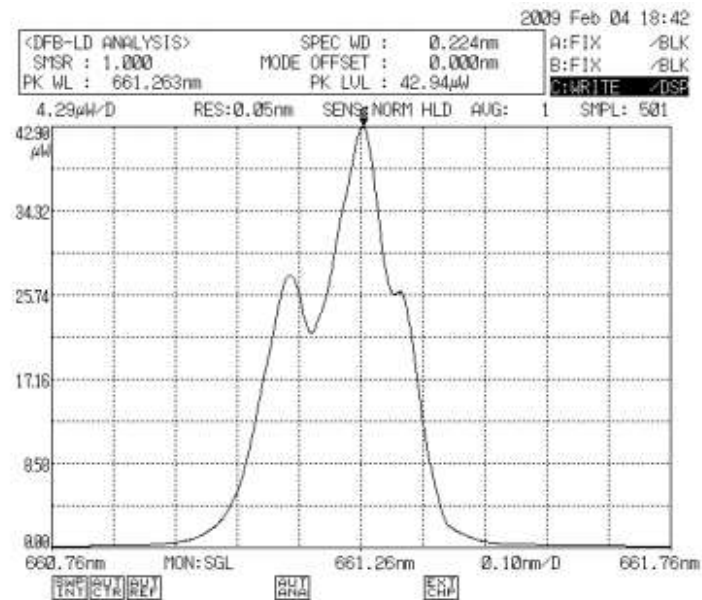
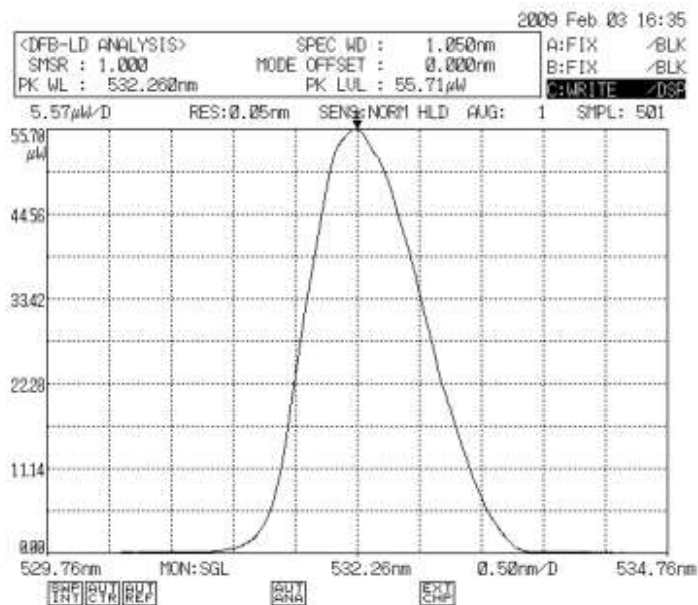
Droga koherencji

$$\Delta L = c \cdot \tau_c = \xi \frac{\lambda^2}{\Delta\lambda}$$

Coherence length

	λ	$\Delta\lambda$	$\Delta L \sim \lambda^2 / \Delta\lambda$
White light	550 nm	750 nm	1 μ m
LED	850 nm	30 nm \div 50 nm	24 \div 15 μ m
	1300 nm	50 nm \div 100 nm	34 \div 17 μ m
SLD	850 nm	150 nm	5 μ m
	1300 nm	60 nm	28 μ m
LD	670 nm	0.2 nm \div 2 nm	2.3 mm \div 230 μ m
	1300 nm	<2 nm	1mm \div 50m
	1550 nm	<2 nm	1mm \div 50m
He-Ne	632.8 nm	<<0.1 nm	0.1m \div 100m
	1152 nm	<<0.1 nm	0.1m \div 300m

Light sources

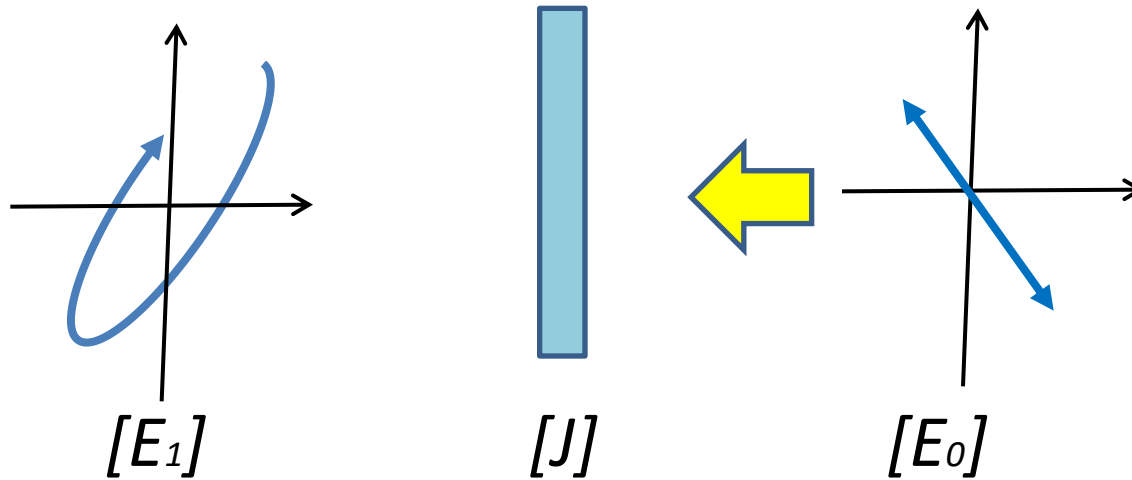


Methods of describing state of polarization changes

Types of descriptions

- Trigonometric method (time consuming)
- Jones's matrix method,
- Muellera's matrix method,
- **Double complex functions method,**

Jones's matrix



$$[E_1] = [J][E_0]$$

$$[E_1] = \begin{bmatrix} j_{11} & j_{12} \\ j_{21} & j_{22} \end{bmatrix} [E_0]$$

Jones's matrix

$$[E_1] = \begin{bmatrix} j_{11} & j_{12} \\ j_{21} & j_{22} \end{bmatrix} [E_0]$$

$$E_{1x} = j_{11}E_{0x} + j_{12}E_{0y}$$

$$E_{1y} = j_{21}E_{0x} + j_{22}E_{0y}$$

Jones's matrix

General form (according to Ścierański and Ratajczyk)

- Can be applied to:
 - dichroic media,
 - Nondichroic absorbing media,

$$[J] = \begin{bmatrix} T_f \cos^2 \beta_f + T_s \sin^2 \beta_f e^{-i\gamma} & \sin \beta_f \cos \beta_f (T_f - T_s e^{-i\gamma}) e^{-i\delta_f} \\ \sin \beta_f \cos \beta_f (T_f - T_s e^{-i\gamma}) e^{i\delta_f} & T_f \sin^2 \beta_f + T_s \cos^2 \beta_f e^{-i\gamma} \end{bmatrix},$$

T_f – fast wave transmittance,

T_s – slow wave transmittance,

γ – phase difference in birefringent medium,

β_f – diagonal angle for fast wave,

δ_f – phase difference defining SOP of the fast wave,

Jones's matrix

- According to Jones

$$[J] = \begin{bmatrix} \cos^2 \beta_f + \sin^2 \beta_f e^{-i\gamma} & \sin \beta_f \cos \beta_f (1 - e^{-i\gamma}) e^{-i\delta_f} \\ \sin \beta_f \cos \beta_f (1 - e^{-i\gamma}) e^{i\delta_f} & \sin^2 \beta_f + \cos^2 \beta_f e^{-i\gamma} \end{bmatrix}.$$

Can be applied to:

- nonabsorbing media,
- Nondichroic waveplates,

Jones's matrix

- Examples:

For free space $\begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix}$

Right-handed circular polarizer $\frac{1}{2} \begin{bmatrix} 1 & i \\ -i & 1 \end{bmatrix}$

For isotropic medium with transmittance p $\begin{bmatrix} p & 0 \\ 0 & p \end{bmatrix}$

Left-handed circular polarizer $\frac{1}{2} \begin{bmatrix} 1 & -i \\ i & 1 \end{bmatrix}$

Linear polarizer, azimuth 0 $\begin{bmatrix} 1 & 0 \\ 0 & 0 \end{bmatrix}$

QWR with fast axis at 0 $\begin{bmatrix} e^{i\pi/4} & 0 \\ 0 & e^{-i\pi/4} \end{bmatrix}$

Linear polarizer, azimuth 90 $\begin{bmatrix} 0 & 0 \\ 0 & 1 \end{bmatrix}$

HWR with fast axis at 45 $\begin{bmatrix} 0 & 1 \\ 1 & 0 \end{bmatrix}$

Linear polarizer, azimuth 45 $\frac{1}{2} \begin{bmatrix} 1 & 1 \\ 1 & 1 \end{bmatrix}$

Wave plate with phase shift δ and fast axis at 0 $\begin{bmatrix} e^{i\delta} \cos^2 \theta + \sin^2 \theta & (e^{i\delta} - 1) \sin \theta \cos \theta \\ (e^{i\delta} - 1) \sin \theta \cos \theta & e^{i\delta} \sin^2 \theta + \cos^2 \theta \end{bmatrix}$

Jones's matrix

Example:

Linearly polarized light passing through QWR:

$$[E] = \frac{1}{\sqrt{2}} \begin{bmatrix} e^{-i\pi/4} & e^{i\pi/4} \\ e^{i\pi/4} & e^{-i\pi/4} \end{bmatrix} \begin{bmatrix} 1 \\ 0 \end{bmatrix} = \frac{1}{\sqrt{2}} \begin{bmatrix} e^{-i\pi/4} \\ e^{i\pi/4} \end{bmatrix}.$$

- Can be applied only for completely polarized light.
- Jones's vectors for natural light or partially polarized does not exist,

Muellers' matrix

$$[S] = [M][S_0]$$

$$\begin{bmatrix} S_0 \\ S_1 \\ S_2 \\ S_3 \end{bmatrix} = \begin{bmatrix} m_{11} & m_{12} & m_{13} & m_{14} \\ m_{21} & m_{22} & m_{23} & m_{24} \\ m_{31} & m_{32} & m_{33} & m_{34} \\ m_{41} & m_{42} & m_{43} & m_{44} \end{bmatrix} \begin{bmatrix} S_{00} \\ S_{01} \\ S_{02} \\ S_{03} \end{bmatrix}$$

Mueller matrix

According to Ścierski – for dichroic media

$$[M] = \begin{bmatrix} T^+ & MT^- & CT^- & ST^- \\ MT^- & M^2Z + X & CMZ + YS & SMZ - YC \\ CT^- & MCZ - YS & C^2Z + X & SCZ + YM \\ ST^- & MSZ + YC & CSZ - YM & S^2Z + X \end{bmatrix}$$

T – transmittance of the amplitude

$$\begin{aligned} T^+ &= (T_f^2 + T_s^2)/2, & M &= \cos 2\vartheta_f \cos 2\alpha_f, \\ T^- &= (T_f^2 - T_s^2)/2, & C &= \cos 2\vartheta_f \sin 2\alpha_f, \\ X &= T_f T_s \cos \gamma, & S &= \sin 2\vartheta_f, \\ Y &= T_f T_s \sin \gamma, & Z &= T^+ - X. \end{aligned}$$

Mueller matrix

For free space

$$\begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

Absorbing medium
with transmittance k

$$\begin{bmatrix} k & 0 & 0 & 0 \\ 0 & k & 0 & 0 \\ 0 & 0 & k & 0 \\ 0 & 0 & 0 & k \end{bmatrix}$$

Linear polarizer with
azimuth θ

$$\frac{1}{2} \begin{bmatrix} 1 & \cos 2\theta & \sin 2\theta & 0 \\ \cos 2\theta & \cos^2 2\theta & \cos 2\theta \sin 2\theta & 0 \\ \sin 2\theta & \cos 2\theta \sin 2\theta & \sin^2 2\theta & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

Mueller matrix

Linear polarizer
with azimuth 0

$$\frac{1}{2} \begin{bmatrix} 1 & 1 & 0 & 0 \\ 1 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix}$$

Linear polarizer
with azimuth 90

$$\frac{1}{2} \begin{bmatrix} 1 & -1 & 0 & 0 \\ -1 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix}$$

Linear polarizer
with azimuth 45

$$\frac{1}{2} \begin{bmatrix} 1 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 \\ 1 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix}$$

Mueller matrix

For wave-plate with azimuth θ and phase retardation δ

$$\begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & \cos^2 2\theta + \sin^2 2\theta \cos \delta & (1 - \cos \delta) \sin 2\theta \cos 2\theta & -\sin 2\theta \sin \delta \\ 0 & (1 - \cos \delta) \sin 2\theta \cos 2\theta & \sin^2 2\theta + \cos^2 2\theta \cos \delta & \cos 2\theta \sin \delta \\ 0 & \sin 2\theta \sin \delta & -\cos 2\theta \sin \delta & \cos \delta \end{bmatrix}$$

QWR with
azimuth 0

$$\begin{pmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 1 \\ 0 & 0 & -1 & 0 \end{pmatrix}$$

QWR with
azimuth 45

$$\begin{pmatrix} 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & -1 \\ 0 & 0 & 1 & 0 \\ 0 & 1 & 0 & 0 \end{pmatrix}$$

QWR with
azimuth -45

$$\begin{pmatrix} 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 \\ 0 & 0 & 1 & 0 \\ 0 & -1 & 0 & 0 \end{pmatrix}$$

QWR with
azimuth 90

$$\begin{pmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & -1 \\ 0 & 0 & 1 & 0 \end{pmatrix}$$

Mueller matrix

For wave-plate with azimuth θ and phase retardation δ

$$\begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & \cos^2 2\theta + \sin^2 2\theta \cos \delta & (1 - \cos \delta) \sin 2\theta \cos 2\theta & -\sin 2\theta \sin \delta \\ 0 & (1 - \cos \delta) \sin 2\theta \cos 2\theta & \sin^2 2\theta + \cos^2 2\theta \cos \delta & \cos 2\theta \sin \delta \\ 0 & \sin 2\theta \sin \delta & -\cos 2\theta \sin \delta & \cos \delta \end{bmatrix}$$

HWR with
azimuth 0

$$\begin{pmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & -1 & 0 \\ 0 & 0 & 0 & -1 \end{pmatrix}$$

HWR with
azimuth 22,5

$$\begin{pmatrix} 1 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & -1 \end{pmatrix}$$

HWR with
azimuth -22,5

$$\begin{pmatrix} 1 & 0 & 0 & 0 \\ 0 & 0 & -1 & 0 \\ 0 & -1 & 0 & 0 \\ 0 & 0 & 0 & -1 \end{pmatrix}$$

HWR with
azimuth 45

$$\begin{pmatrix} 1 & 0 & 0 & 0 \\ 0 & -1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & -1 \end{pmatrix}$$

Mueller's matrix

$$[M_{\alpha_0+\alpha}] = [T_{-\alpha}] [M_{\alpha_0}] [T_{\alpha}],$$

$$[T_{-\alpha}] = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & \cos 2\alpha & -\sin 2\alpha & 0 \\ 0 & \sin 2\alpha & \cos 2\alpha & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix}$$

$$[T_{\alpha}] = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & \cos 2\alpha & \sin 2\alpha & 0 \\ 0 & -\sin 2\alpha & \cos 2\alpha & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix}$$

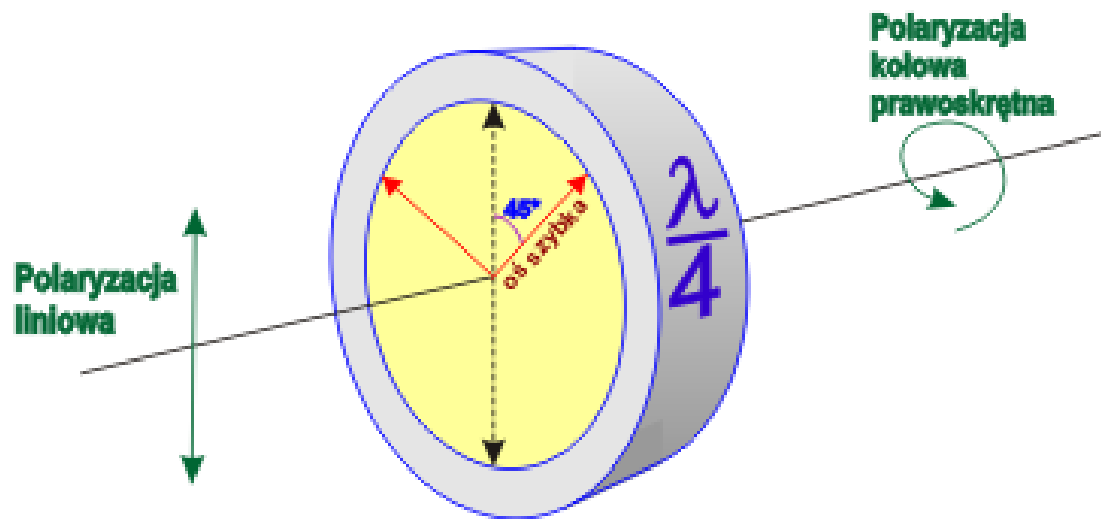
Mueller's matrix

- Example

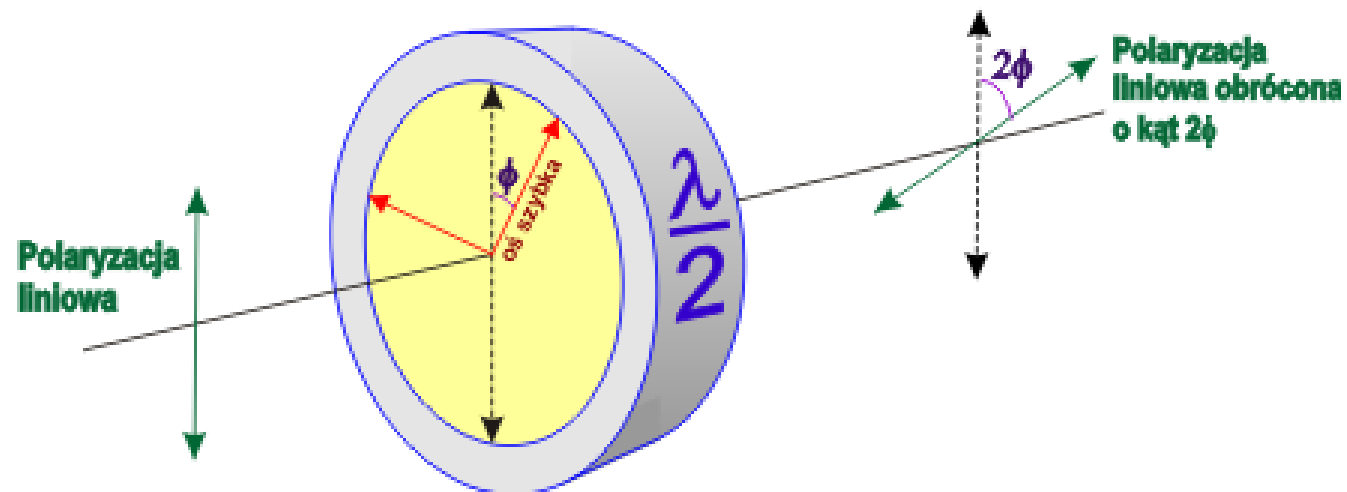
A depolarized light passing through polarizer and QWR

$$[S] = \begin{array}{c} \text{ćwierćfalówka} \\ \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & -1 \\ 0 & 0 & 1 & 0 \\ 0 & 1 & 0 & 0 \end{bmatrix} \end{array} \frac{1}{2} \begin{array}{c} \text{polaryzator} \\ \begin{bmatrix} 1 & 1 & 0 & 0 \\ 1 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix} \end{array} \begin{array}{c} \text{światło} \\ \text{naturalne} \\ \begin{bmatrix} 1 \\ 0 \\ 0 \\ 0 \end{bmatrix} \end{array} = \begin{array}{c} \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & -1 \\ 0 & 0 & 1 & 0 \\ 0 & 1 & 0 & 0 \end{bmatrix} \end{array} \frac{1}{2} \begin{array}{c} \begin{bmatrix} 1 \\ 1 \\ 0 \\ 0 \end{bmatrix} \end{array} = \frac{1}{2} \begin{array}{c} \begin{bmatrix} 1 \\ 0 \\ 0 \\ 1 \end{bmatrix} \end{array}$$

Ćwierćfalówka przesuwają fazę składowych o ćwierć długości fali.

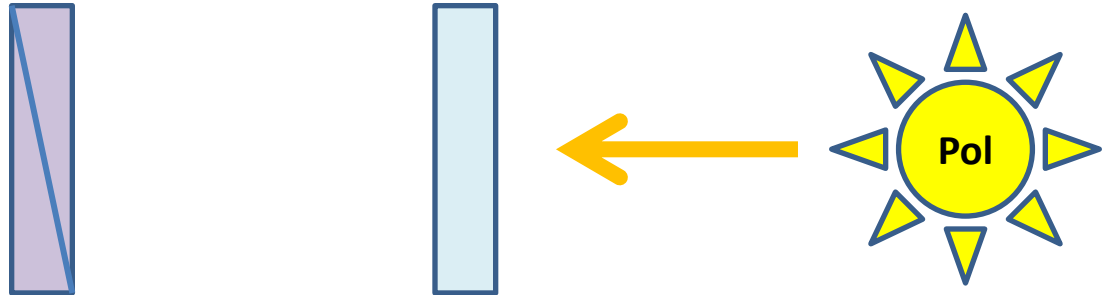


Półfalówka przesuwają fazę składowych o pół długości fali.



Task

1. How to estimate experimentally fast and slow axis of the waveplate using linear polarizer and linearly polarized light beam? Can we distinguish fast and slow axis?



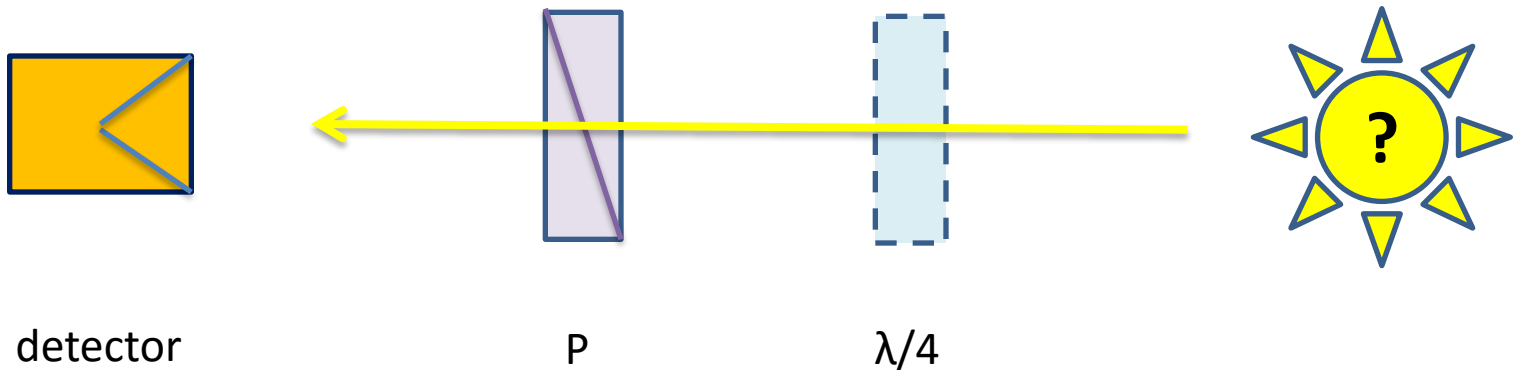
$$\begin{bmatrix} S_0 \\ S_1 \\ S_2 \\ S_3 \end{bmatrix} = \frac{1}{2} \begin{bmatrix} 1 & 1 & 0 & 0 \\ 1 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix} \cdot \begin{bmatrix} m_{11} & m_{12} & m_{13} & m_{14} \\ m_{21} & m_{22} & m_{23} & m_{24} \\ m_{31} & m_{32} & m_{33} & m_{34} \\ m_{41} & m_{42} & m_{43} & m_{44} \end{bmatrix} \cdot \begin{bmatrix} 1 \\ 1 \\ 0 \\ 0 \end{bmatrix}$$

Methods of measuring SOP

- 6 (or 4) light intensity measurements using polarizer and QWR,
- Method based on circular polarizer,
- Rotating QWR method,
- Null-intensity method,

Method 1

QWR and linear polarizer,
6 light intensities with different configurations of P and QWR.



$$[S] = \begin{bmatrix} S_0 \\ S_1 \\ S_2 \\ S_3 \end{bmatrix} = \sqrt{\frac{\mu_0}{\epsilon_0}} \begin{bmatrix} I_{(0,0^\circ)} + I_{(0,90^\circ)} \\ I_{(0,0^\circ)} - I_{(0,90^\circ)} \\ I_{(0,45^\circ)} - I_{(0,135^\circ)} \\ I_{\left(\frac{\lambda}{4},45^\circ\right)} - I_{\left(\frac{\lambda}{4},135^\circ\right)} \end{bmatrix}.$$

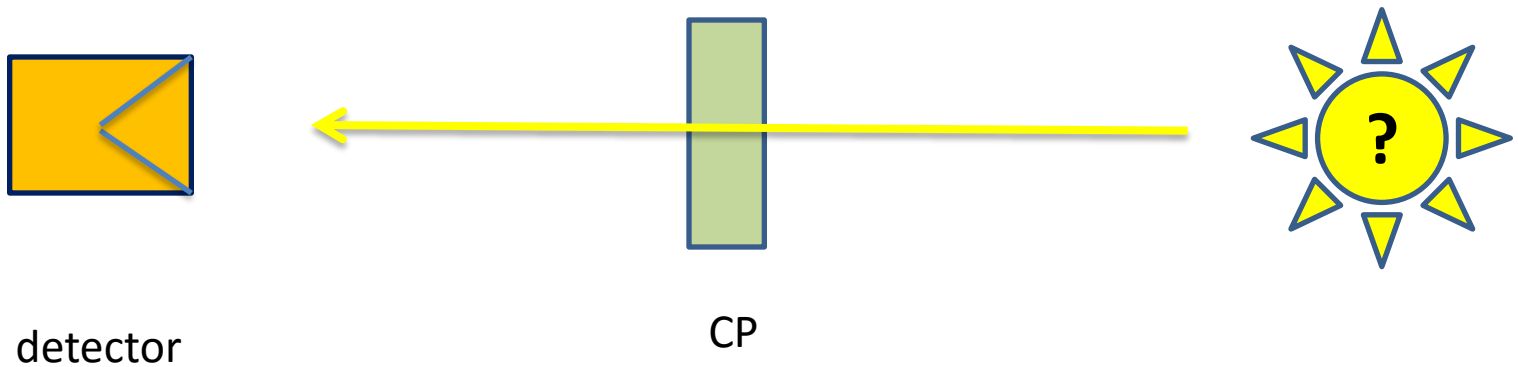
Method 1

- 6 measurements can be simplified to 4 measurements:

$$[S] = \begin{bmatrix} S_0 \\ S_1 \\ S_2 \\ S_3 \end{bmatrix} = \sqrt{\frac{\mu_0}{\epsilon_0}} \begin{bmatrix} I_{(0,0^\circ)} + I_{(0,90^\circ)} \\ I_{(0,0^\circ)} - I_{(0,90^\circ)} \\ 2I_{(0,45^\circ)} - I_{(0,0^\circ)} - I_{(0,90^\circ)} \\ 2I_{\left(\frac{\lambda}{4}, 45^\circ\right)} - I_{(0,0^\circ)} - I_{(0,90^\circ)} \end{bmatrix}$$

Method 2

- Using circular polarizer

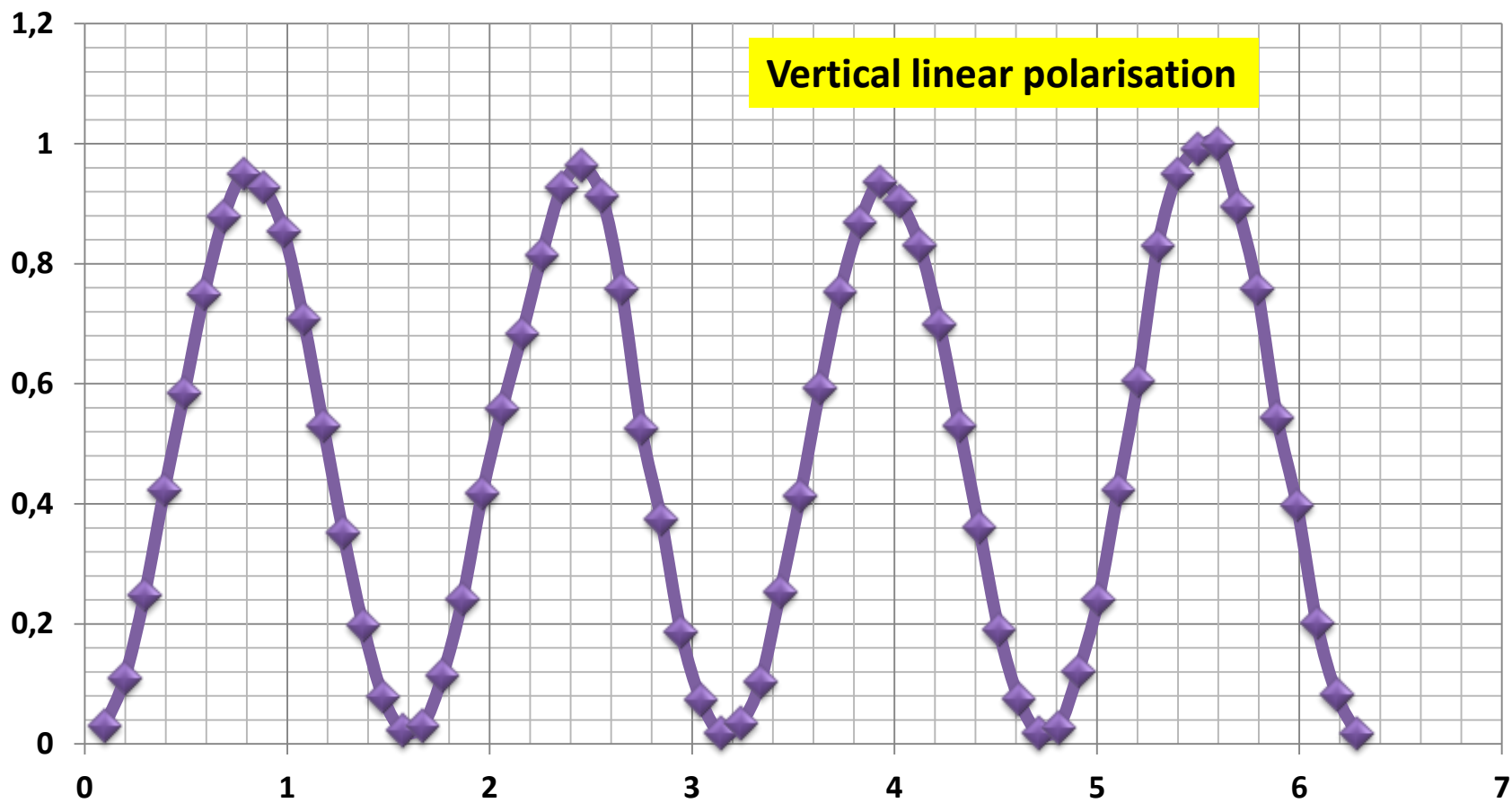


$$[S] = \begin{bmatrix} S_0 \\ S_1 \\ S_2 \\ S_3 \end{bmatrix} = \begin{bmatrix} I_c(0^\circ) + I_c(90^\circ) \\ S_0 - 2I_c(45^\circ) \\ I_c(0^\circ) - I_c(90^\circ) \\ S_0 - 2I_L(0^\circ) \end{bmatrix}$$

Method 3

- Rotating QWR,
 - Commonly used in commercial devices,





Method 3

$$S(x) = \frac{a_0}{2} + \sum_{n=1}^{\infty} \left(a_n \cos \left(\frac{2n\pi}{T}x \right) + b_n \sin \left(\frac{2n\pi}{T}x \right) \right)$$

where:

$$a_n = \frac{2}{T} \int_{-\frac{T}{2}}^{\frac{T}{2}} f(x) \cos \left(\frac{2n\pi}{T}x \right) dx, \quad n = 0, 1, 2, \dots$$

$$b_n = \frac{2}{T} \int_{-\frac{T}{2}}^{\frac{T}{2}} f(x) \sin \left(\frac{2n\pi}{T}x \right) dx, \quad n = 1, 2, 3, \dots$$

$$[S] = \begin{bmatrix} S_0 \\ S_1 \\ S_2 \\ S_3 \end{bmatrix} = \begin{bmatrix} \frac{1}{2}a_0 - a_4 \\ 2a_4 \\ 2b_4 \\ b_2 \end{bmatrix}$$